

## A study on copper corrosion and its effect on dielectric properties of paper oil insulation of transformers using simulation and laboratory experiments

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*This study investigates the impact of copper sulphide which is formed due to corrosive sulphur in mineral oil on dielectric properties of paper oil insulation of model transformer windings. The effect of copper sulphide on electric stress distribution is explained using FEM based electric field computations. frequency domain spectroscopy and insulation resistance measurements were carried out on the prototype transformer windings under conditions of copper corrosion at different temperatures and the variations in  $\tan \delta$ , real and imaginary part of complex permittivity ( $\epsilon'$ ,  $\epsilon''$ ), insulation resistance, and polarization index are discussed.*

**Keywords:** Copper sulphide, DBDS, paper oil insulation, transformer,  $\tan \delta$ , permittivity, insulation resistance, polarization index.

### 1.0 INTRODUCTION

Paper-oil insulation plays an important role in determining the performance and life span of the power transformers, reactors, etc,. In recent years, quality of mineral oil insulation and the major changes it undergoes during its service life have been carefully monitored to understand the health of the transformer and to prevent failures that are triggered by degradation of mineral oil. In recent past, many cases of transformer failures due to formation of semiconducting copper sulphide in paper insulation are reported [1-3]. The corrosive sulphur compounds in mineral oil react on copper conductors under certain conditions and this results in the formation and migration of copper sulphide ( $\text{Cu}_2\text{S}$ ) towards inner paper layers.

### 2.0 CHEMISTRY OF COPPER CORROSION

Dibenzyl Disulphide (DBDS) is an anti-oxidant and anti-wear additive which is used in

transformer oil to improve its performance. In presence of DBDS, mineral oil becomes corrosive at higher temperatures and this leads to  $\text{Cu}_2\text{S}$  formation and it is followed by its migration into the paper layers [4-5]. DBDS reacts with copper ions forming a copper-organic compound. This DBDS-Copper complex decomposes and results in the formation of copper sulphide and other by-products [5]. Thus building up of  $\text{Cu}_2\text{S}$  on paper starts and it is forced into inner layers of paper.

### 3.0 EFFECT OF $\text{Cu}_2\text{S}$ ON DIELECTRIC PARAMETERS

It is reported that  $\text{Cu}_2\text{S}$  is a semi-conductor which is widely used in photovoltaic applications [6]. The semi-conductive nature of  $\text{Cu}_2\text{S}$  is observed in the temperature range of 300 K to 383 K and it becomes conductive above 383 K [6]. When  $\text{Cu}_2\text{S}$  gets deposited on kraft paper, it tends to change the dielectric properties of paper insulation. It is also documented that the resistivity of  $\text{Cu}_2\text{S}$

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contaminated paper decreases with temperature and moisture [7].

$\text{Cu}_2\text{S}$  has the tendency to distort the electric stress in the paper insulation and it enhances the electric stress at certain locations. When  $\text{Cu}_2\text{S}$  migrates into inner paper layers, it will lead to significant increase in leakage current,  $\tan \delta$  and it also alters the electric stress distribution resulting in inception of electrical discharges around  $\text{Cu}_2\text{S}$  sites [7]. This can also trigger turn to turn flashovers in the windings and finally end up in the breakdown of insulation system.

In the larger perspective of preventive maintenance of in-service power transformers, it is necessary to understand the dielectric performance of paper oil insulation when formation and progressive migration of  $\text{Cu}_2\text{S}$  into the paper insulation takes place. This study attempts to understand the dielectric parameters of paper oil insulation in presence of  $\text{Cu}_2\text{S}$ . The distribution of electric stress in  $\text{Cu}_2\text{S}$  contaminated paper insulation of model transformer winding is studied using Finite Element Method (FEM) and the results are presented in this paper. This paper also presents results of Frequency Domain Spectroscopy (FDS) and Insulation Resistance (IR) on laboratory model of transformer windings contaminated by  $\text{Cu}_2\text{S}$ . The measurements were carried out at temperatures of  $25^\circ\text{C}$ ,  $90^\circ\text{C}$  and  $140^\circ\text{C}$ . The effect of both temperature and extent of copper sulphide contamination on the dielectric performance of paper oil insulation is explained.

#### 4.0 SIMULATION STUDY ON EFFECTS OF $\text{Cu}_2\text{S}$

In this study, electric field simulations were carried out on a pigtail sample configuration as shown in Figure 1. It consists of two paper covered copper conductors which are tightly held together by PTFE tape. Each copper conductor has four layers of paper each of  $55\ \mu\text{m}$  thickness. FEM simulation is confined to the straight portion of pigtail sample. The boundary conditions are  $V=1$  at HV conductor and  $V=0$  at LV conductor.

FEM simulations are carried out by representing the clean impregnated paper layer by its relative permittivity of 3.75. With the complete deposition of  $\text{Cu}_2\text{S}$  on the first layer, it is assigned a permittivity of 40 and different conductivity values of  $1 \times 10^{-15}\ \text{S/m}$  and  $1 \times 10^{-4}\ \text{S/m}$  are assigned in order to represent its semiconducting and metallic nature and these values are based on published data [7].

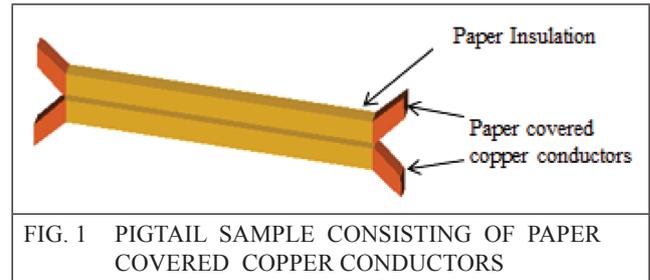


FIG. 1 PIGTAIL SAMPLE CONSISTING OF PAPER COVERED COPPER CONDUCTORS

It is assumed that  $\text{Cu}_2\text{S}$  is initially formed on the conductor surface and then it migrates to the first paper layer and sequentially to inner paper layers on High Voltage (HV) conductor and then sequentially onto the Low Voltage (LV) conductor of the pigtail sample. Under these assumptions, electric field simulation has been performed for the following cases:

- $\text{Cu}_2\text{S}$  with conductivity of  $1 \times 10^{-15}\ \text{S/m}$  and  $\epsilon_r = 40$  (Lower conductivity, temperature  $< 383\ \text{K}$ ).
- $\text{Cu}_2\text{S}$  with conductivity of  $1 \times 10^{-4}\ \text{S/m}$  and  $\epsilon_r = 40$  (Higher conductivity, temperature  $> 383\ \text{K}$ ).

The electric stress (E) in clean paper is observed to be  $2.28\ \text{V/mm}$  for an input voltage of 1V. The electric stress is also computed for progressive migration of  $\text{Cu}_2\text{S}$  and the values of electric stress in the clean and  $\text{Cu}_2\text{S}$  contaminated paper layers for different values of conductivity of  $\text{Cu}_2\text{S}$  are furnished under Table 1 and 2.

From Table 1 and 2 it is observed that the increase in electric stress is not significant during the initial stages of  $\text{Cu}_2\text{S}$  migration. But, when migration of  $\text{Cu}_2\text{S}$  takes place into second, third and subsequent layers, there is a considerable increase in electric stress across

clean paper layers. This is much severe in case of Cu<sub>2</sub>S having conductivity of  $\sigma = 10^{-4}$  S/m.

TABLE 1			
ELECTRIC STRESS IN CU <sub>2</sub> S CONTAMINATED AND CLEAN PAPER LAYERS ( $\Sigma = 10^{-15}$ S/M)			
No. of Cu <sub>2</sub> S contaminated paper layers from HV conductor	Maximum Electric Stress (V/mm)		
	E <sub>Cu2S</sub>	E <sub>Clean</sub>	% increase in stress compared to clean case
1	0.24	2.56	12
2	0.27	2.94	29
3	0.32	3.45	51
4	0.39	4.16	82
5	0.50	5.24	130
6	0.67	7.10	211
7	1.03	11.00	382
8	2.28	----	----

TABLE 2			
ELECTRIC STRESS IN CU <sub>2</sub> S CONTAMINATED AND CLEAN PAPER LAYERS ( $\Sigma = 10^{-4}$ S/M)			
No. of Cu <sub>2</sub> S contaminated paper layers from HV conductor	Maximum Electric Stress(V/mm)		
	E <sub>Cu2S</sub>	E <sub>Clean</sub>	% increase in stress compared to clean case
1	0.003	2.60	14
2	0.004	3.03	32
3	0.007	3.64	60
4	0.008	4.54	99
5	0.009	6.05	165
6	0.010	9.05	297
7	0.030	18.00	690
8	2.280	----	----

It is also evident that the electric stress is reduced across Cu<sub>2</sub>S contaminated papers and there is enhancement of electric stress across clean areas of paper. Thus it is expected that higher electric

stress appears across clean paper leading to its breakdown and this is followed by breakdown of Cu<sub>2</sub>S contaminated paper layers. The variation of maximum electric stress (E<sub>max</sub>) across clean paper layers for progressive migration of Cu<sub>2</sub>S for different conductivity values is shown in Figure 2.

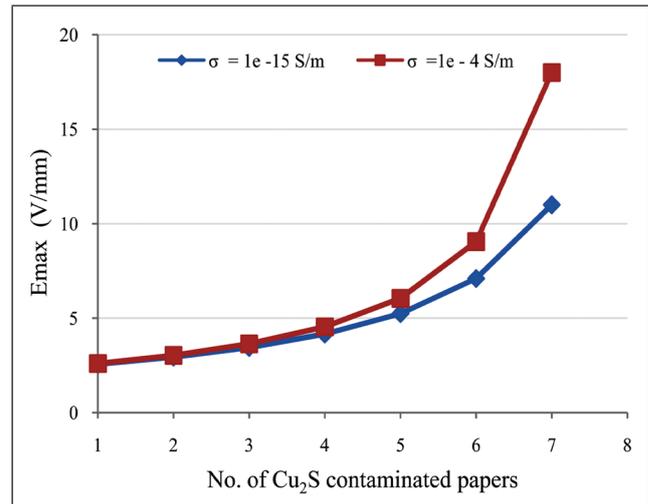


FIG. 2 VARIATION OF MAXIMUM ELECTRIC STRESS ON CLEAN PAPER LAYERS WITH NUMBER OF CU<sub>2</sub>S CONTAMINATED LAYERS

It is interesting to note that migration of Cu<sub>2</sub>S into third and subsequent paper layers results in significant increase of electric stress. In such cases it can exceed dielectric strength of paper insulation and may lead to the complete breakdown of insulation system.

### 5.0 EXPERIMENTAL STUDY

The experimental studies under this investigation were carried out on pigtail samples. The paper layers on the High Voltage (HV) conductor are initially contaminated by Cu<sub>2</sub>S and Low Voltage (LV) conductor is clean. All the samples were initially dried and impregnated with dried and degassed mineral oil by conventional method and each sample was immersed in 500 ml of mineral oil in a sealed container and kept in a temperature controlled oven. The temperature of the oven was preset to 25° C, 90° C and 140° C respectively.

**5.1 Results of FDS Measurements**

FDS measurements were carried out on pigtail samples at 200 V AC over a frequency range of 0.1 mHz to 1 kHz using dielectric response analyser of M/s. Omicron Electronics.

**5.1.1 Effect of Cu<sub>2</sub>S and temperature on tan δ**

The variations of tan δ with frequency in clean and Cu<sub>2</sub>S contaminated paper at 25° C, 90° C and 140° C are shown in Figure 3, 4 and 5.

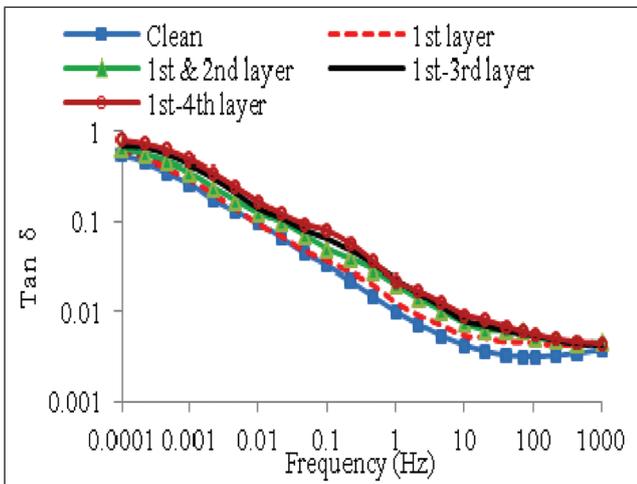


FIG. 3 VARIATION OF TAN Δ WITH FREQUENCY IN CLEAN AND CU2S CONTAMINATED PAPER AT 25° C.

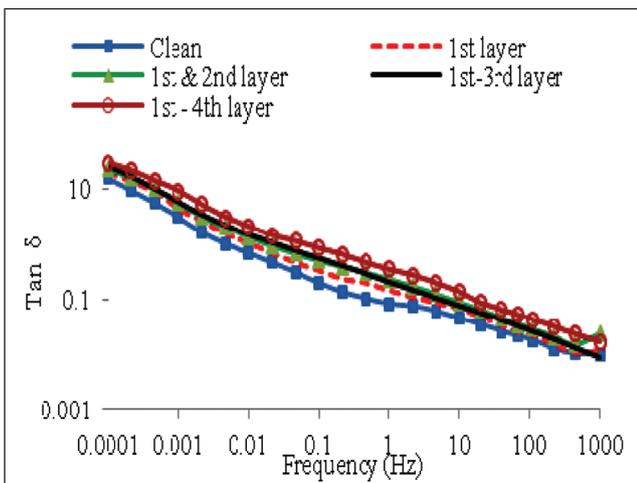


FIG. 4 VARIATION OF TAN Δ WITH FREQUENCY IN CLEAN AND CU2S CONTAMINATED PAPER AT 90° C

It is observed that there is a upward shift in tan δ values with increase in the number of Cu<sub>2</sub>S affected paper layers and this is mainly attributed to Cu<sub>2</sub>S deposits on paper. The minimum of tan δ is observed at 100 Hz for clean paper layer and at higher frequencies for Cu<sub>2</sub>S contaminated layers respectively. It is also seen that there is a logarithmic shift of magnitude of tan δ which is caused by increase in activation energy at higher temperatures [8]. An increasing contribution of conduction mechanisms is indicated by the slope of the tan δ curve at lower frequencies. Hence, temperature appears to be very crucial to the observed results. This becomes more prominent with Cu<sub>2</sub>S deposits.

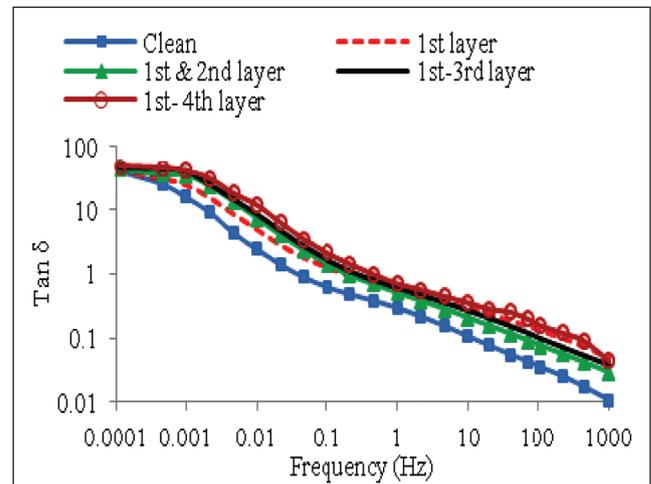


FIG. 5 VARIATION OF TAN Δ WITH FREQUENCY IN CLEAN AND CU2S CONTAMINATED PAPER AT 140° C

**5.1.2 Effect of Cu<sub>2</sub>S and temperature on ε'**

The variations of real part of complex permittivity (ε') with frequency in clean and Cu<sub>2</sub>S contaminated paper at 25° C, 90° C and 140° C are shown in Figure 6, 7 and 8. The results show that there is an increasing trend in ε' with increase in number of Cu<sub>2</sub>S affected paper layers at the low frequency region and variations are very much reduced at middle and higher frequencies at 25° C. On the other hand, at 90° C and 140° C, the variations in ε' are least, at the higher frequencies. There is also significant increase in ε' values at temperatures of 90° C and 140° C.

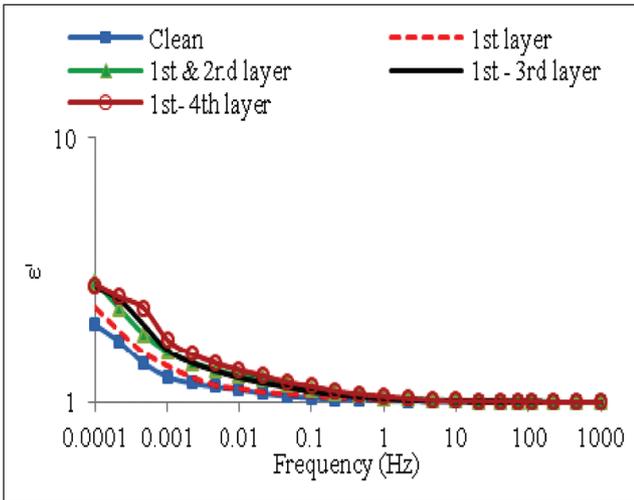


FIG. 6 VARIATION OF  $\epsilon'$  WITH FREQUENCY IN CLEAN AND  $\text{Cu}_2\text{S}$  CONTAMINATED PAPER AT 25° C.

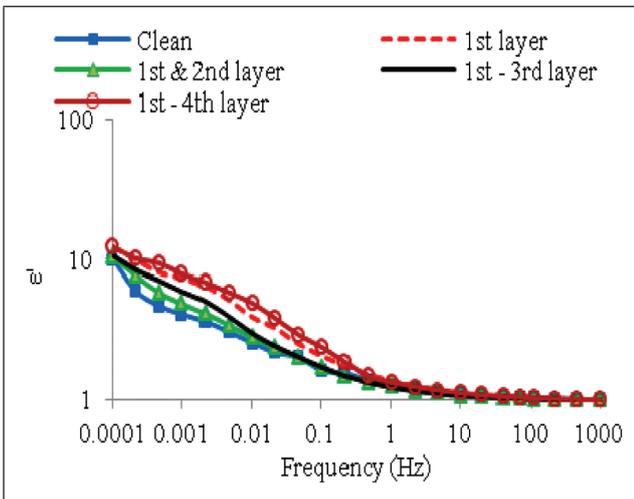


FIG. 7 VARIATION OF  $\epsilon'$  WITH FREQUENCY IN CLEAN AND  $\text{Cu}_2\text{S}$  CONTAMINATED PAPER AT 90° C.

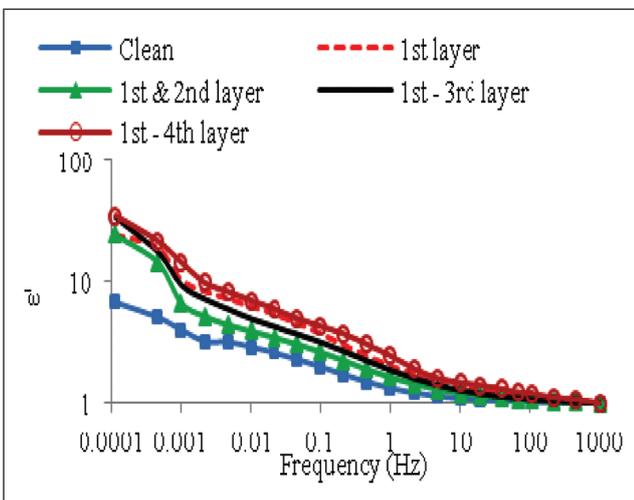


FIG. 8 VARIATION OF  $\epsilon'$  WITH FREQUENCY IN CLEAN AND  $\text{Cu}_2\text{S}$  CONTAMINATED PAPER AT 140° C.

### 5.1.3 Effect of $\text{Cu}_2\text{S}$ and temperature on $\epsilon''$

The variations of imaginary part of complex permittivity ( $\epsilon''$ ) with frequency in clean and  $\text{Cu}_2\text{S}$  contaminated paper at 25° C, 90° C and 140° C are shown in Figure 9, 10 and 11. The variation in  $\epsilon''$  is similar to the  $\tan \delta$  variations. The conductivity of  $\text{Cu}_2\text{S}$  is visible in terms of increase in  $\epsilon''$  and the temperature dependent conductivity of  $\text{Cu}_2\text{S}$  is observed to be more significant at 90° C and 140° C respectively.

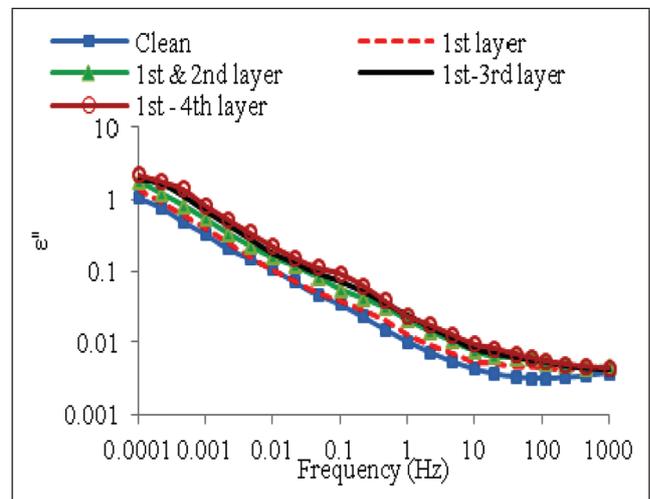


FIG. 9 VARIATION OF  $\epsilon''$  WITH FREQUENCY IN CLEAN AND  $\text{Cu}_2\text{S}$  CONTAMINATED PAPER AT 25° C.

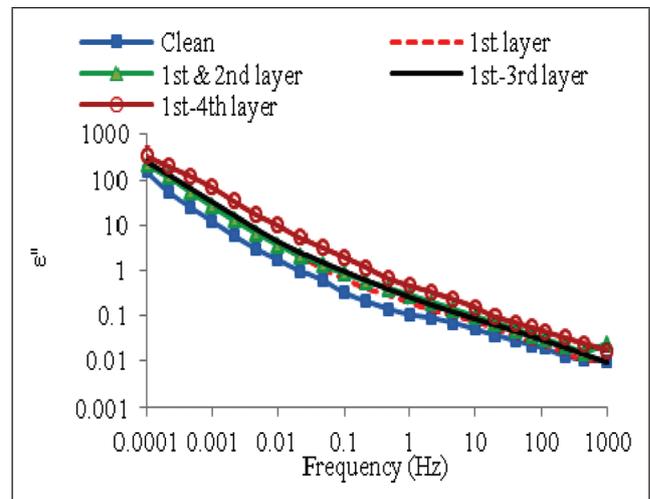


FIG. 10 VARIATION OF  $\epsilon''$  WITH FREQUENCY IN CLEAN AND  $\text{Cu}_2\text{S}$  CONTAMINATED PAPER AT 90° C.

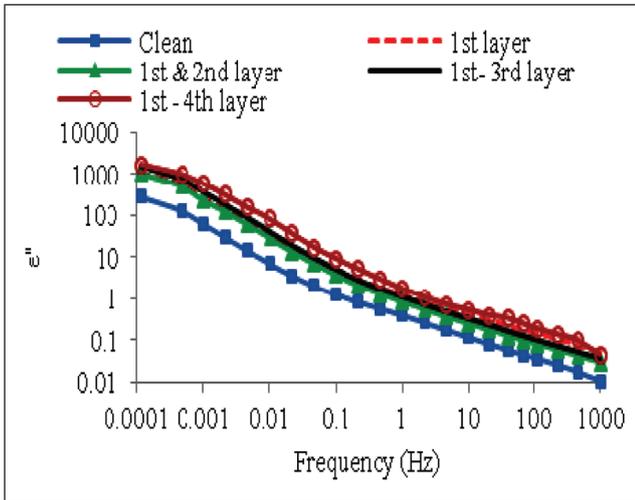


FIG. 11 VARIATION OF  $\epsilon''$  WITH FREQUENCY IN CLEAN AND  $\text{Cu}_2\text{S}$  CONTAMINATED PAPER AT  $140^\circ\text{C}$ .

**5.2 Effect of  $\text{Cu}_2\text{S}$  and temperature on Insulation Resistance**

The values of Insulation resistance (IR) are measured at 500 V for one minute for both clean case and  $\text{Cu}_2\text{S}$  contaminated samples. The measurements are carried out at  $25^\circ\text{C}$ ,  $90^\circ\text{C}$  and  $140^\circ\text{C}$  respectively and the results are shown in Figure 12.

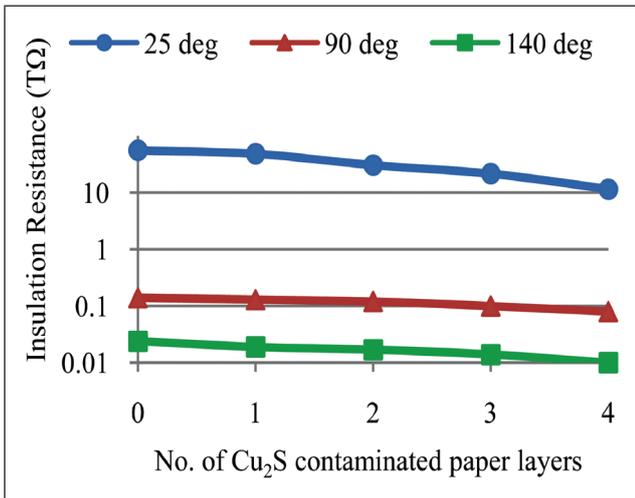


FIG.12 VARIATIONS OF INSULATION RESISTANCE FOR CLEAN AND  $\text{Cu}_2\text{S}$  CONTAMINATED PAPER AT  $25^\circ\text{C}$ ,  $90^\circ\text{C}$  AND  $140^\circ\text{C}$

There is a reduction in the value of insulation resistance with increase in temperature and number of paper layers contaminated by  $\text{Cu}_2\text{S}$ .

**5.3 Effect of  $\text{Cu}_2\text{S}$  and temperature on Polarization Index**

The values of polarization index (PI) calculated from the ratio of 10 minutes IR to 1 minute IR values at 500 V for clean case and  $\text{Cu}_2\text{S}$  contaminated samples at  $25^\circ\text{C}$ ,  $90^\circ\text{C}$  and  $140^\circ\text{C}$  are presented in Table 3. It is observed from Table 3 that the polarization index decreases with increase in temperature and number of paper layers contaminated by  $\text{Cu}_2\text{S}$ . The trend observed in the PI values are similar to IR values and the reduction in PI values are significant at  $90^\circ\text{C}$  and  $140^\circ\text{C}$ .

TABLE 3			
VALUES OF PI FOR CLEAN AND $\text{Cu}_2\text{S}$ CONTAMINATED PAPER LAYERS AT $25^\circ\text{C}$ , $90^\circ\text{C}$ AND $140^\circ\text{C}$			
NO. OF PAPER LAYERS WITH $\text{Cu}_2\text{S}$ ON HV SIDE	At $25^\circ\text{C}$	At $90^\circ\text{C}$	At $140^\circ\text{C}$
0	2.926	1.264	0.971
1	2.868	1.188	0.932
2	2.603	1.041	0.838
3	2.494	0.989	0.649
4	2.272	0.866	0.571

**6.0 CONCLUSION**

The important conclusions of this study are:

1. The effect of  $\text{Cu}_2\text{S}$  migration on paper layers has shown that there is a non uniform electric stress distribution across paper layers. The electric stress is more across the clean paper layers as compared to  $\text{Cu}_2\text{S}$  affected papers.
2. The values of  $\tan \delta$ ,  $\epsilon'$  and  $\epsilon''$  increase in magnitude at higher temperature under  $\text{Cu}_2\text{S}$  contamination.
3. Polarization Index (PI) and Insulation resistance (IR) decrease with increase in temperature and progressive migration of  $\text{Cu}_2\text{S}$ .

Though there are characteristic changes in dielectric parameters under conditions of copper corrosion, it becomes challenging to use the conventional dielectric measurement in actual transformer windings where the insulation geometry is huge. Moreover, dielectric response measurements such as FDS may give confusing or misleading information about the moisture content in the paper when the  $\text{Cu}_2\text{S}$  deposits are present together in paper-oil insulation.

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