# Multiple feedback-control-loops for single-phase full-bridge PWM inverter

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This paper presents a multiple feedback-loop-control technique for a single-phase full-bridge PWM inverter with output LC filter. The main challenge for an Uninterruptible Power Supply (UPS) is to maintain a high quality sinusoidal voltage under non-linear load conditions as most of the electronic loads are non-linear in nature and for that it needs to be controlled. Multiple feedback consists of two control-loops; one for capacitor voltage and other for inductor current-control. Output voltage and load curren-feedforward-control is used. This technique reduces the distortion in the inverter output voltage and brings it closer to a sine wave. The control concept has been verified using Matlab/Simulink<sup>TM</sup> toolbox and the simulation results are obtained with different types of loads.

*Keywords:* UPS, analog control, feed forward control

## **1.0 INTRODUCTION**

Uninterruptible power supplies are widely used for the continuity and quality in the supply of electric power to sensitive loads, like computer systems, medical equipments, telecommunication systems, in power line problems [1]. The main aim of the UPS system is to provide a high quality sinusoidal output voltage with low total harmonic distortion. A clean sinusoidal output voltage is achieved by using a Sinusoidal Pulse Width Modulation (SPWM) technique and LC filter at the output side of the inverter. But, with non-linear load, the PWM scheme does not guarantee low distortion in the load voltage. There is significant increase in the utility voltage distortions because of the growing use of non-linear loads by industrial, commercial and residential consumers. To mitigate the effects caused by non-linear loads on the utility system, feedback controllers are used.

There are many control topologies for the single phase UPS inverters. At present, many feedback

control techniques are available to control the inverter output voltage [2]-[6]. This paper presents a voltage and current-control scheme for the inverter stage of the UPS. Two control-loops are included in this controller, an inner inductor current-control-loop and an outer capacitor voltage-control-loop.

# 2.0 OPEN LOOP INVERTER

The basic topology of the single-phase full-bridge PWM inverter with LC filter and load is shown in Figure 1. The system variables and parameters are defined in Table 1.

Unipolar SPWM scheme is used to create proper gating signals for the inverter switches as this method effectively doubles the switching frequency of the inverter voltage, making the output LC filter smaller and cheaper. The output voltage of the bridge can be  $+V_{DC}$ ,  $-V_{DC}$  or zero depending on how the switches are controlled.

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The output voltage is switched either from  $+V_{DC}$  to zero or form  $-V_{DC}$  to zero.



TABLE 1	
DEFINITION OF SYSTEM VARIABLES AND	
PARAMETERS	
Var.	Definition
V <sub>DC</sub>	DC Bus voltage
Co	DC link capacitor
$i_L$	Current through filter inductor
i_*	Reference inductor current
Vc	Voltage across filter capacitor
v <sub>c</sub> *	Reference capacitor voltage
i <sub>c</sub>	Current through filter capacitor
i <sub>c</sub> *	Reference capacitor current
$i_{LOAD}$	Load current
m*	Reference signal to PWM modulator
VI	Full-bridge output voltage
K <sub>inv</sub>	Inverter gain

Figure 2 shows the inverter output voltage and current waveform in case of non-linear load i.e. diode rectifier with capacitor filter with 80 % modulation index. We can see that the load current of the inverter deviates significantly from the sinusoidal nature. This distorted current leads to distortion in the inverter output voltage which is not desirable at all. It is necessary to get the desirable sinusoidal voltage with low THD for any kind of load. So, we are using feedback controller to regulate the output voltage of the inverter.



### 3.0 VOLTAGE AND CURRENT CONTROLLER



Figure 3 shows the block diagram of the inverter with controller. The controller used here is a PI controller. The function of the voltage-controlloop is to set the output voltage to the output voltage reference value. The actual output voltage is compared with the reference output voltage and the error signal is given to the PI voltage controller. The controller processes this error. If the actual output voltage is less than the reference voltage, it will increase the current limit reference as the voltage controller output is used as inductor current reference [7-11]. The current controller minimizes the error between the measured inductor current and the reference current. The output of the current controller is the reference signal to the PWM modulator required for the generation of gating signals to the inverter switches. If the feedback current is less than the reference current, the controller increases the reference signal i.e. duty of the switches till it meets the required current value. For a given voltage control, the inner current-control-loop will execute till  $i_L=i_L*$ . So the inner control-loop should be faster than the outer control-loop.

The complete plant and controller modeling block diagram of the inverter is shown in Figure 4. Here, the inverter gain is assumed as unity so that  $m^* = v_I$ .



#### 4.0 DESIGN OF CURRENT-LOOP

Let us consider only current-loop of the inverter. The current controller controls  $i_L$  by controlling  $v_L$ . Here,  $v_c$  acts as disturbance. The current controller has to unnecessarily generate  $v_c$ . The output voltage disturbance  $v_c$  is compensated through output voltage feed forward as shown in Figure 5 so that the controller needs to generate only  $v_L^*$ . Figure 6 gives the simplified current-loop which shows that the current-loop is independent of the output voltage disturbance.





The closed loop transfer function of the current loop is given as:

$$\frac{i_{L}(s)}{i_{L}^{*}(s)} = \frac{K_{I}(1+sT_{I})}{s^{2}LT_{I}+sT_{I}K_{I}+K_{I}} \qquad \dots (1)$$

Comparing this with standard 2<sup>nd</sup> order system, we get,

$$K_I = 2\xi \omega_n L \text{ and } T_I = \frac{2\xi}{\omega_n} \qquad \dots (2)$$

#### 5.0 DESIGN OF VOLTAGE-LOOP

Now, consider the voltage-loop of the inverter. Let the current-loop is ideal ( $i_L = i_L^*$ ). The voltage controller controls the output voltage  $v_c$  by controlling  $i_c$ . Here, the load current acts as disturbance. The voltage controller needs to unnecessarily generate  $i_{LOAD}$ . The load current disturbance is compensated through load current-feedforward as shown in Figure 7 so that the controller needs to generate only  $i_c^*$ . The simplified voltage-loop of the inverter is given in Figure 8 which shows that it is free from the load current disturbance.



The closed loop transfer function of the voltageloop is given as:

$$\frac{v_{c}(s)}{v_{c}^{*}(s)} = \frac{K_{v}(1 + sT_{v})}{s^{2}CT_{v} + sT_{v}K_{v} + K_{v}}$$
....(3)

Comparing this with standard 2<sup>nd</sup> order system, we get,

$$K_v = 2\xi \omega_n C$$
 and  $T_v = \frac{2\xi}{\omega_n}$  ....(4)

We have to tune these parameters till the actual waveform exactly follows the reference waveform. The values of  $\xi$  and  $\omega_n$  depend on the system's required settling time and the allowable peak overshoot.

#### 6.0 SIMULATION RESULTS

The design parameters for the inverter are L = 580 mH, C = 4.7  $\mu$ F, Switching frequency, f<sub>sw</sub> =25 kHz. The simulation is done using MATLAB/ Simulink<sup>TM</sup> toolbox. The solver used is ode4 (Runge-Kutta) with fixed step size of 0.1  $\mu$ s. The results are obtained with 1500 W load.

The output voltage waveforms of the inverter for non-linear (diode bridge rectifier with capacitor filter) as well as linear (R, RL and RC) loads are shown in Figure 9 to Figure 12.









# 7.0 CONCLUSION

The output voltage waveform of the inverter with non-linear load is significantly improved when the controller is used. For any kind of load, even though there is sudden change in load, the output voltage of the inverter remains constant at the desired voltage with low THD value if the controller is used.

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